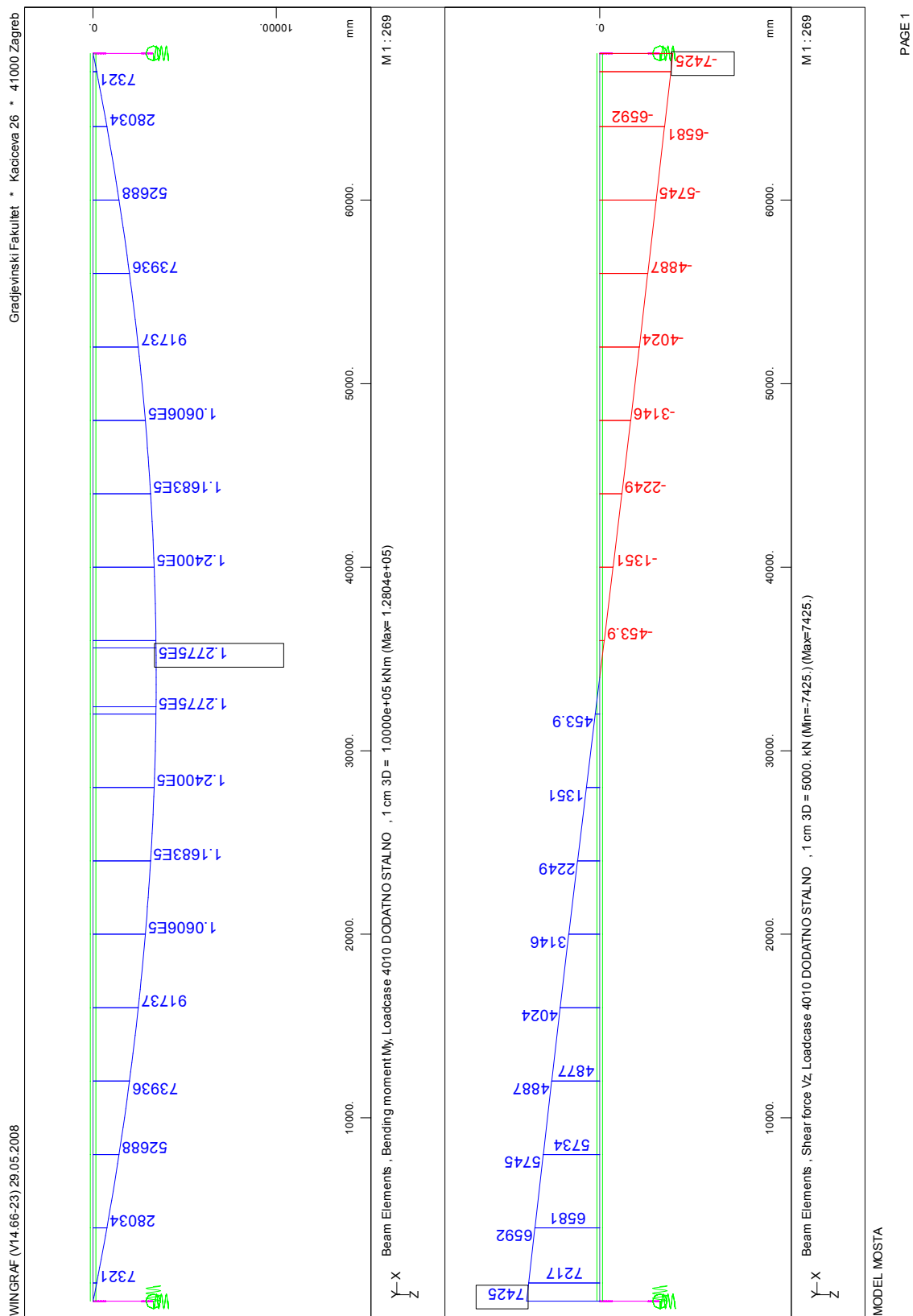
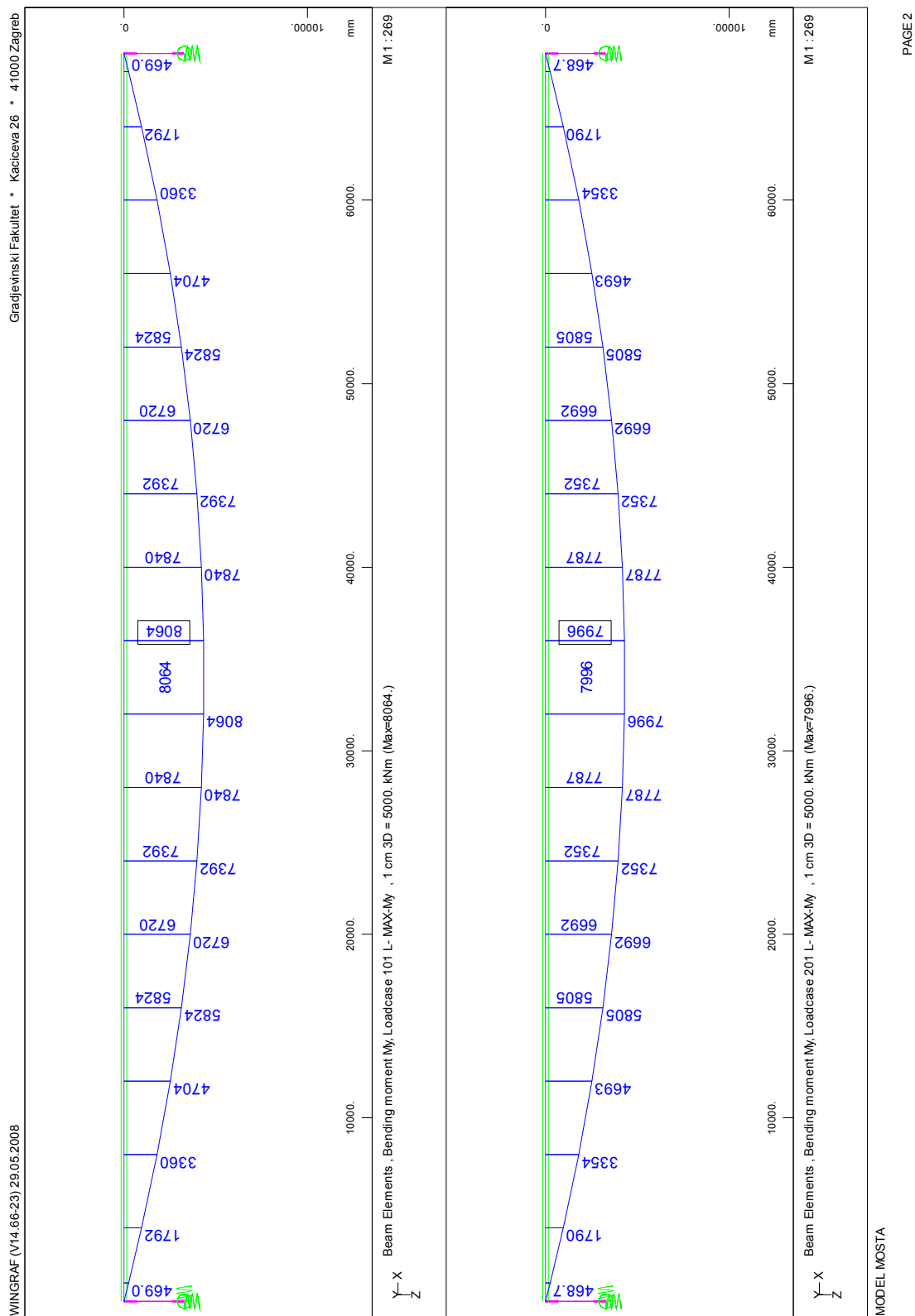


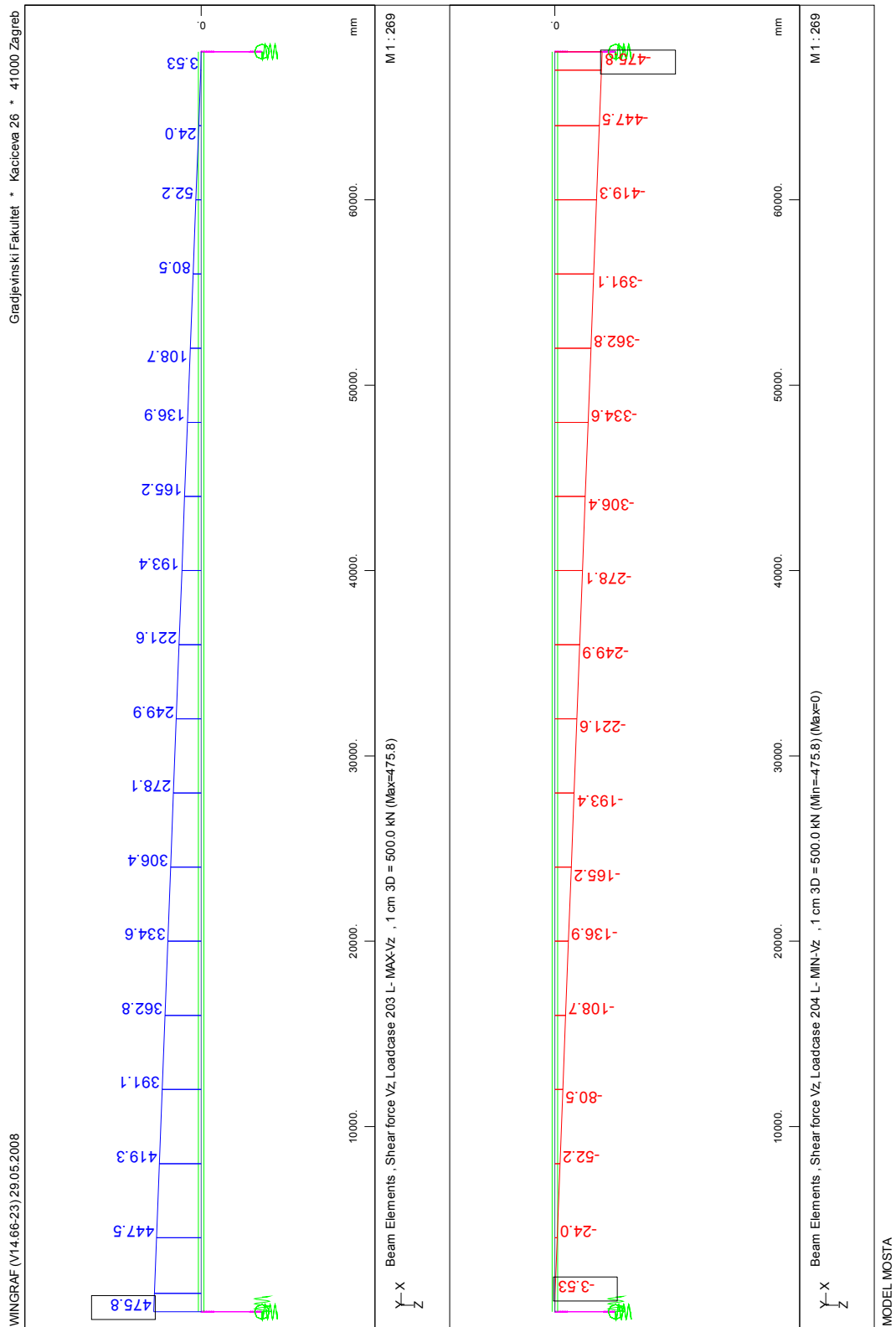
REZULTATI PRORAČUNA IZ SOFISTIKA



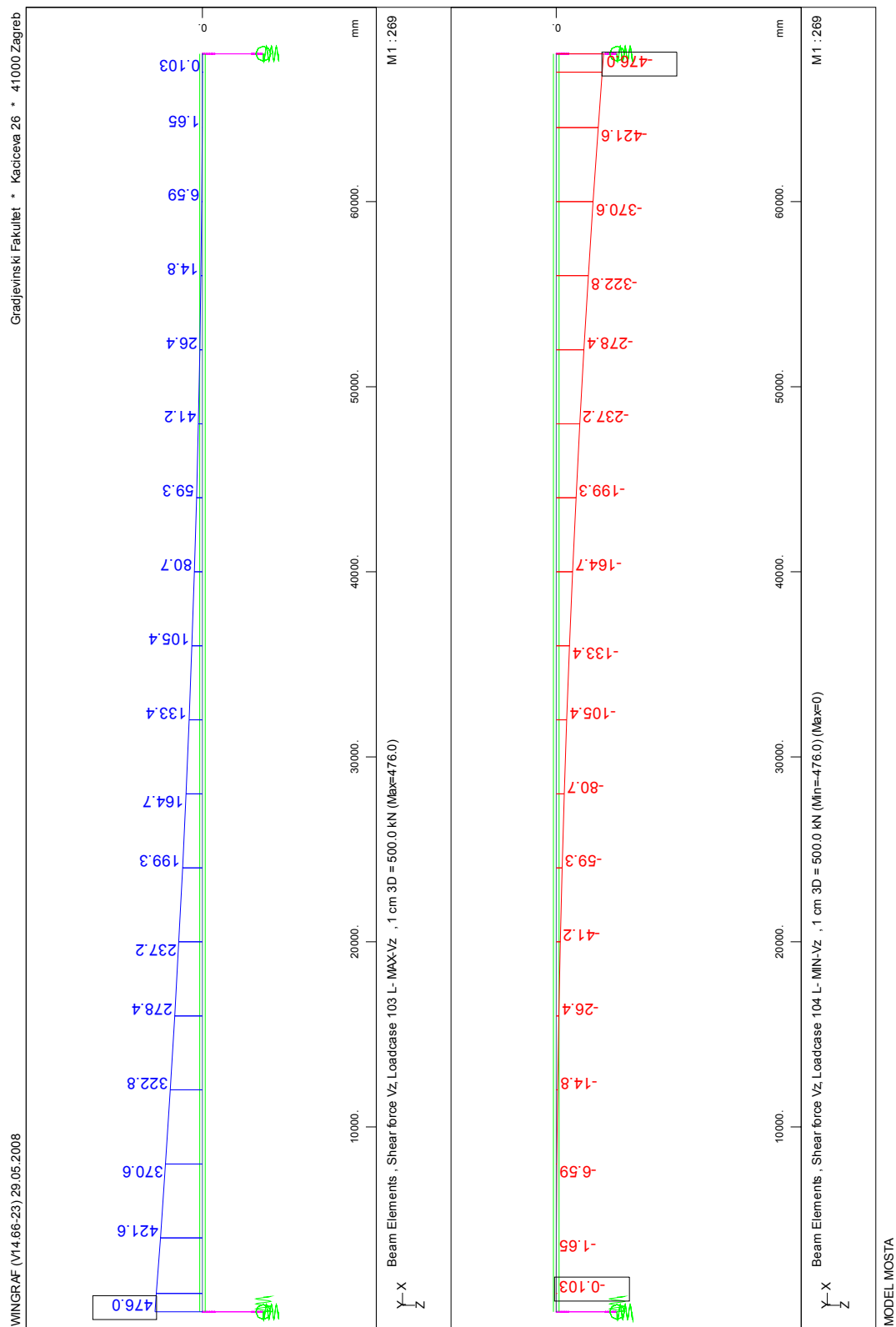
Moment savijanja i poprečne sile: stalno + dodatno stalno



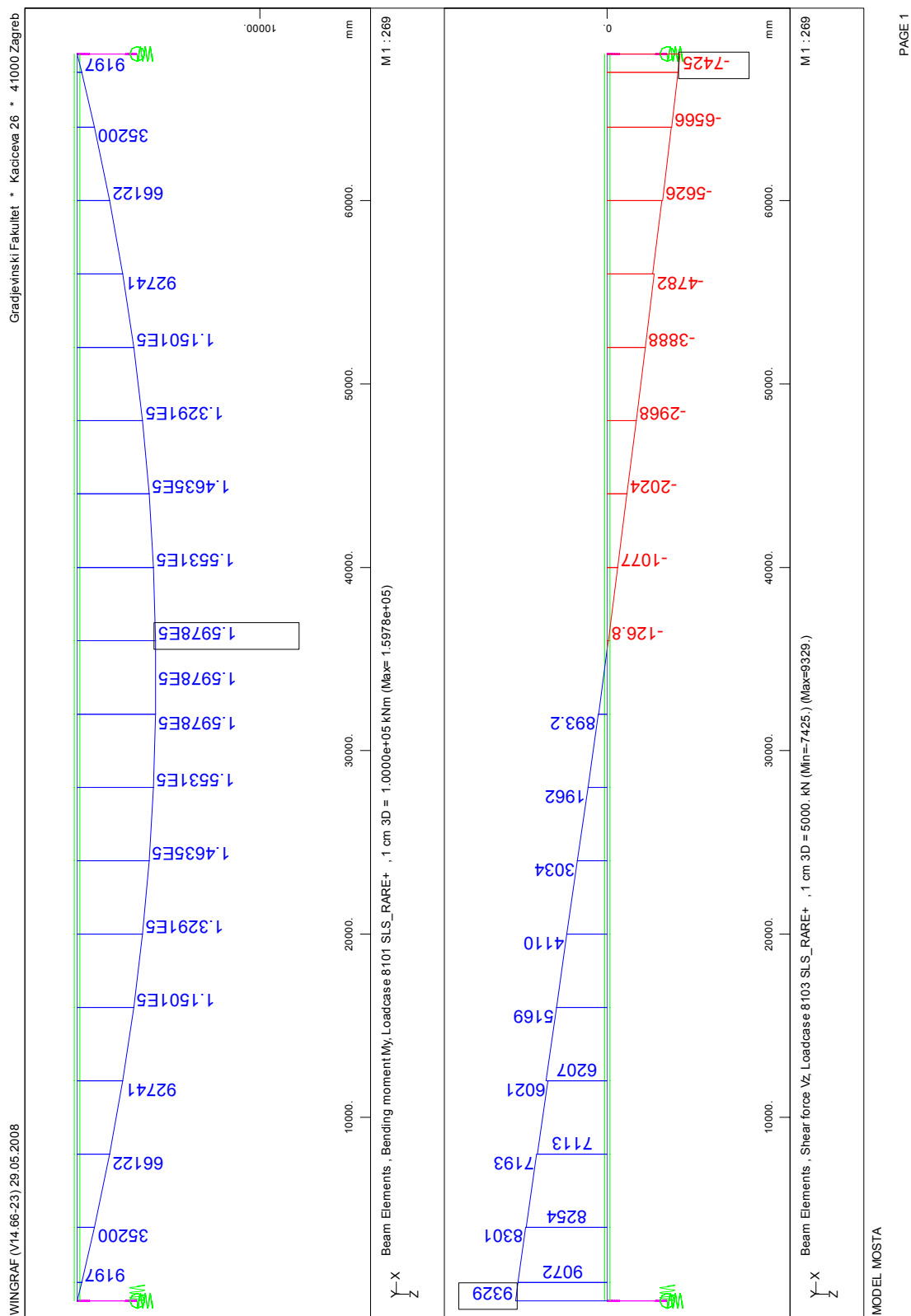
Moment savijanja za prometno opt: Kontinuirano, koncentrirano



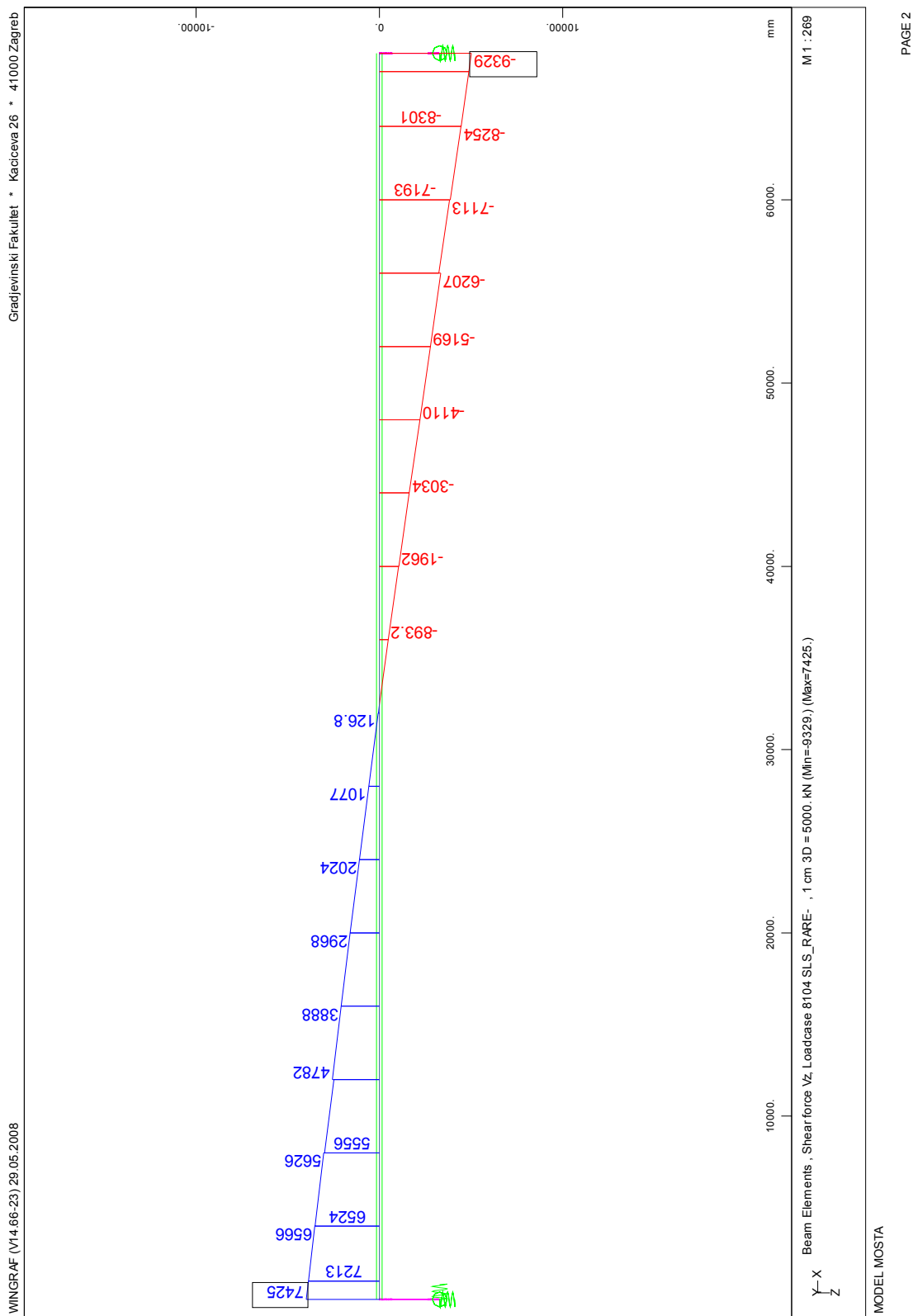
Poprečne sile za prometno opt: kontinuirano



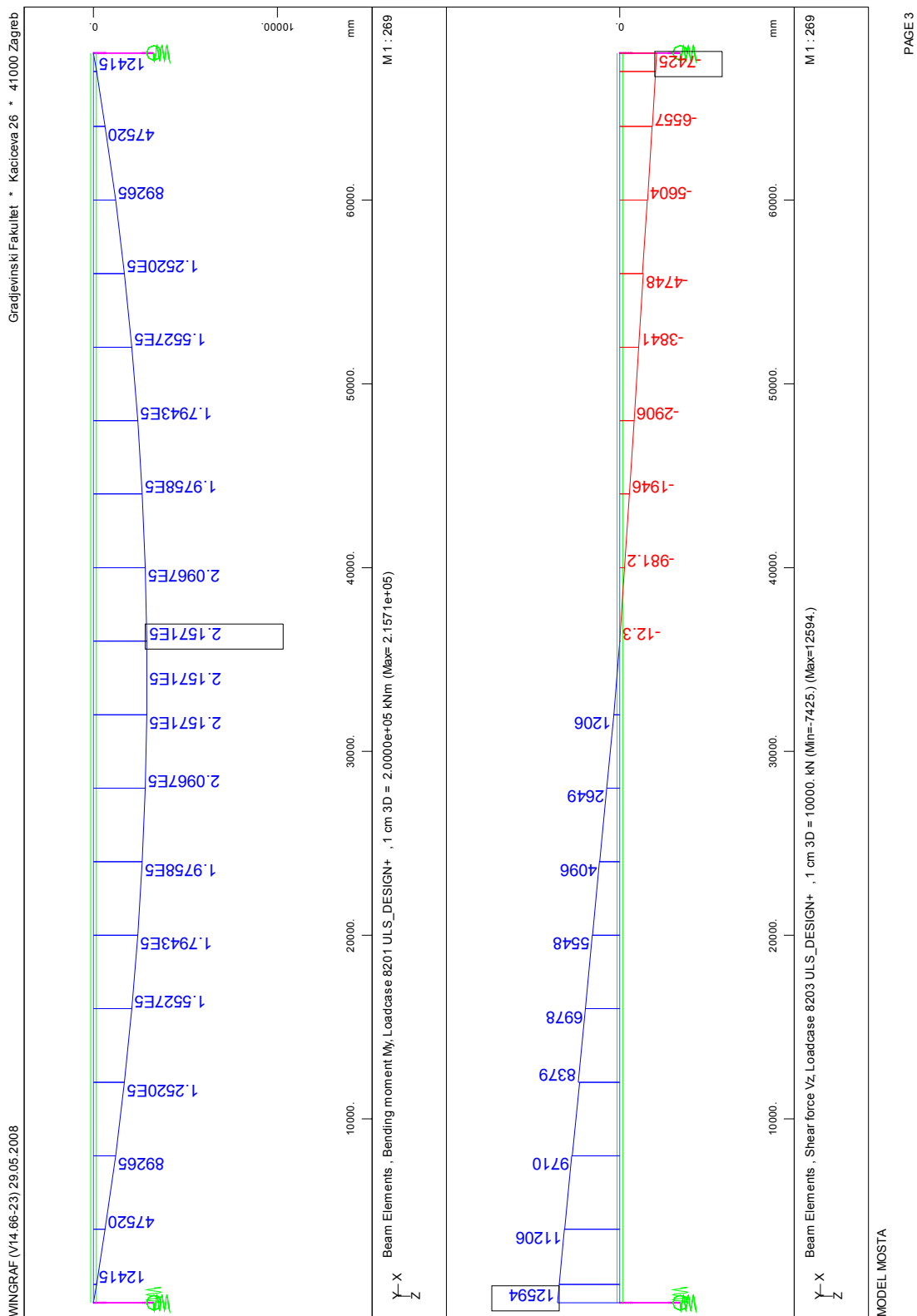
Poprečne sile za prometno opt: koncentrirano



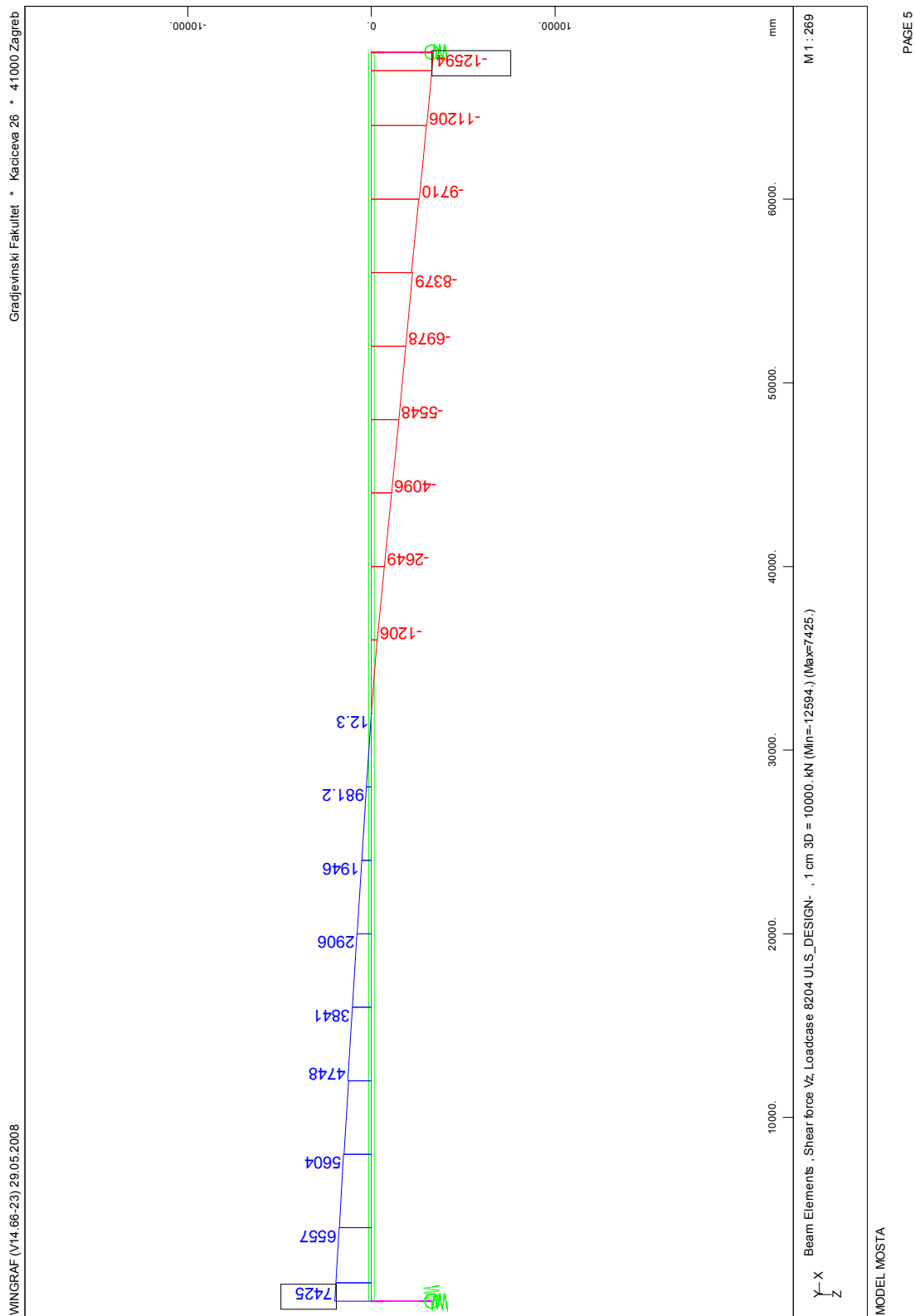
Moment i poprečna sila za GSU (SLS): rijetka kombinacija



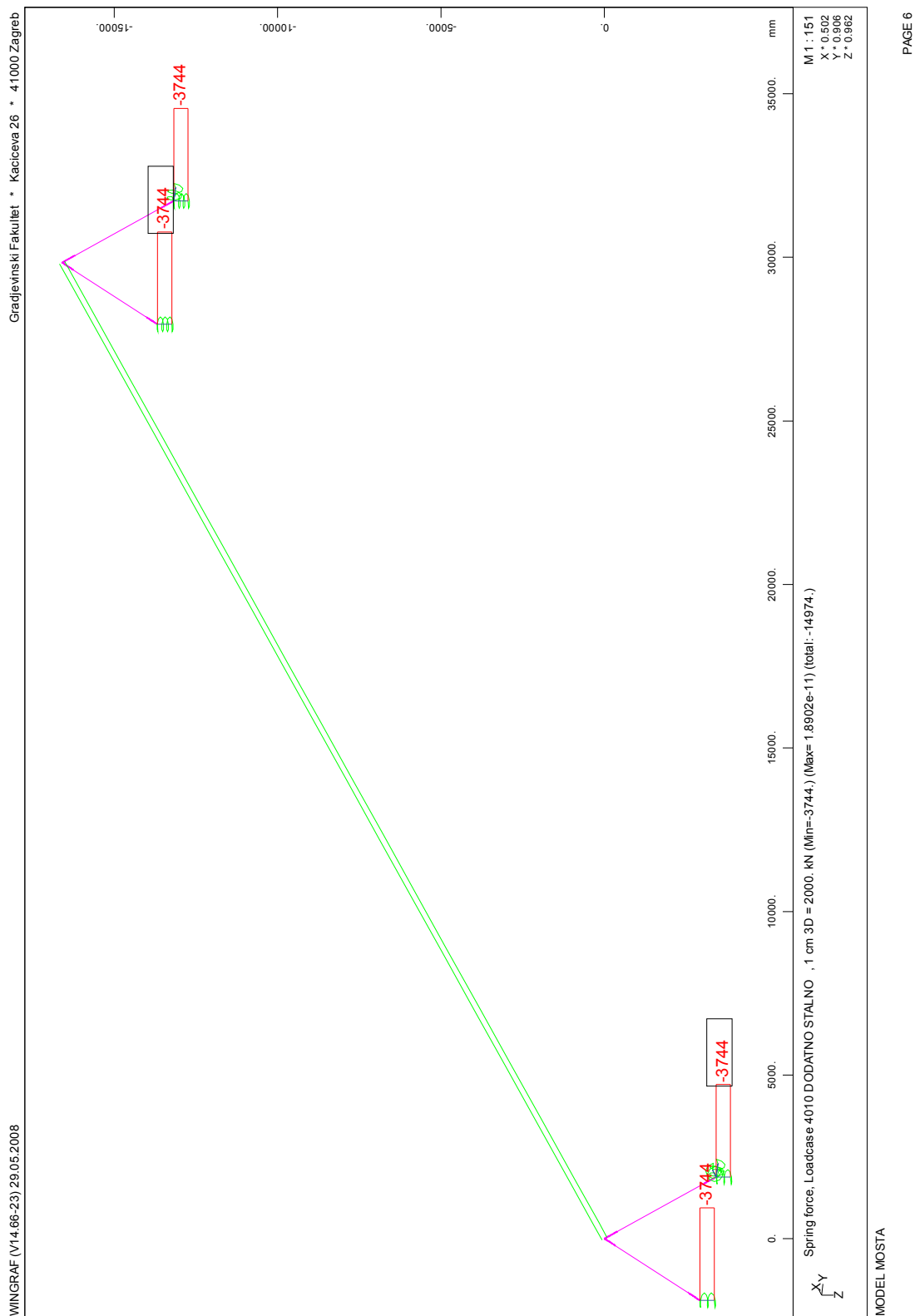
Poprečna sila za GSU (SLS): rijetka kombinacija



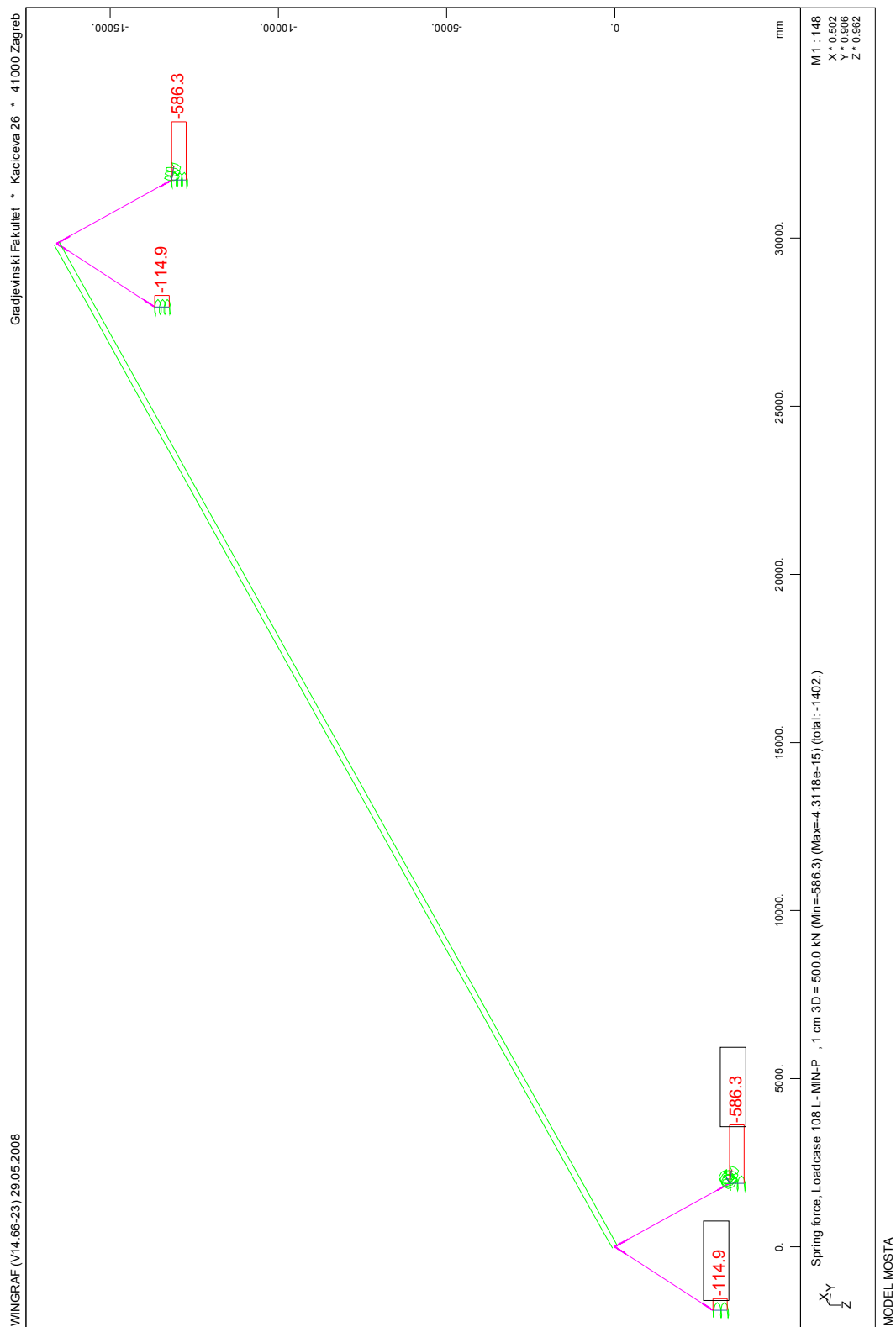
Moment i poprečna sila za GSN (ULS)

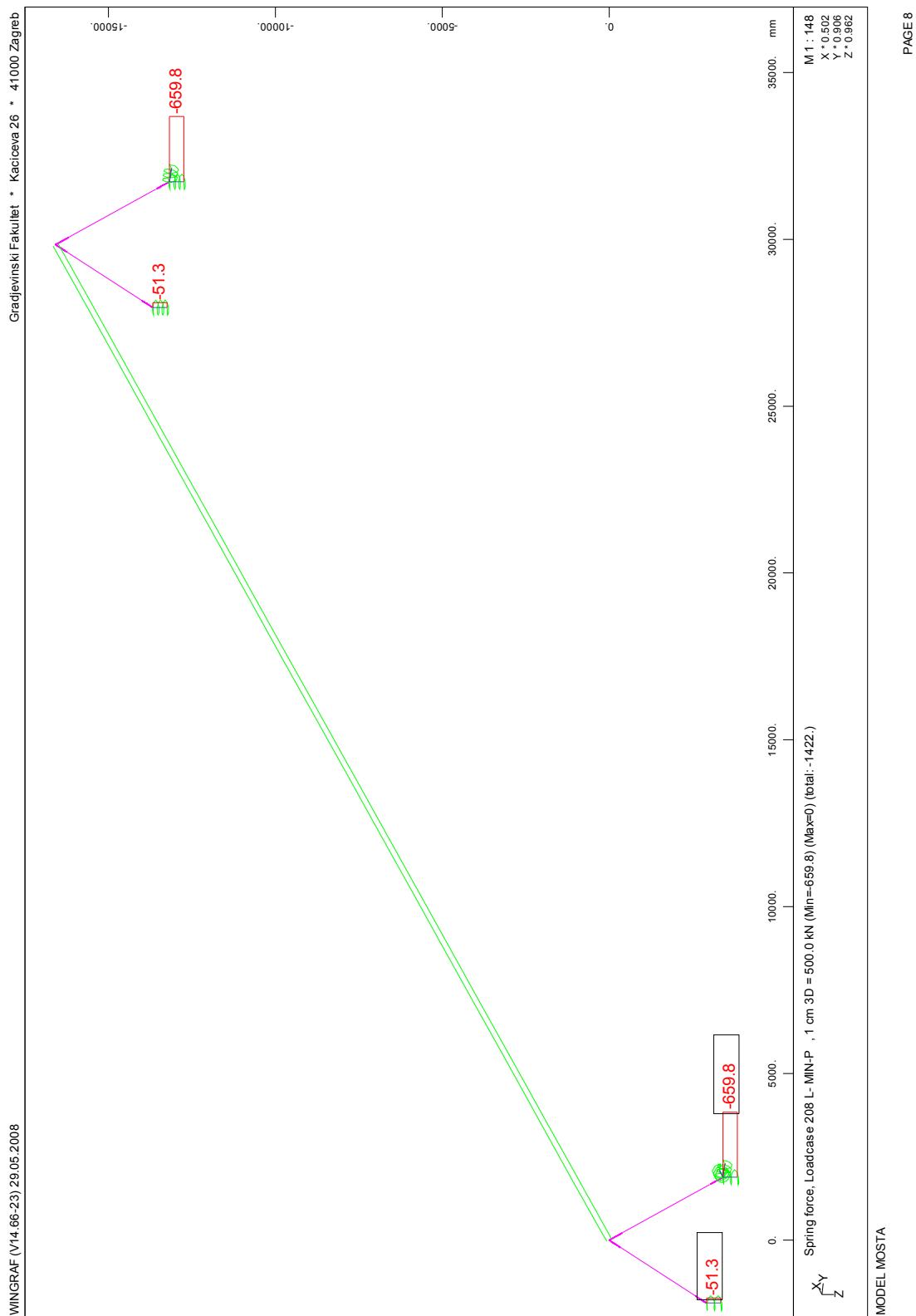


Poprečna sila za GSN (ULS): rijetka kombinacija

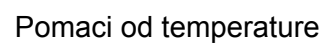


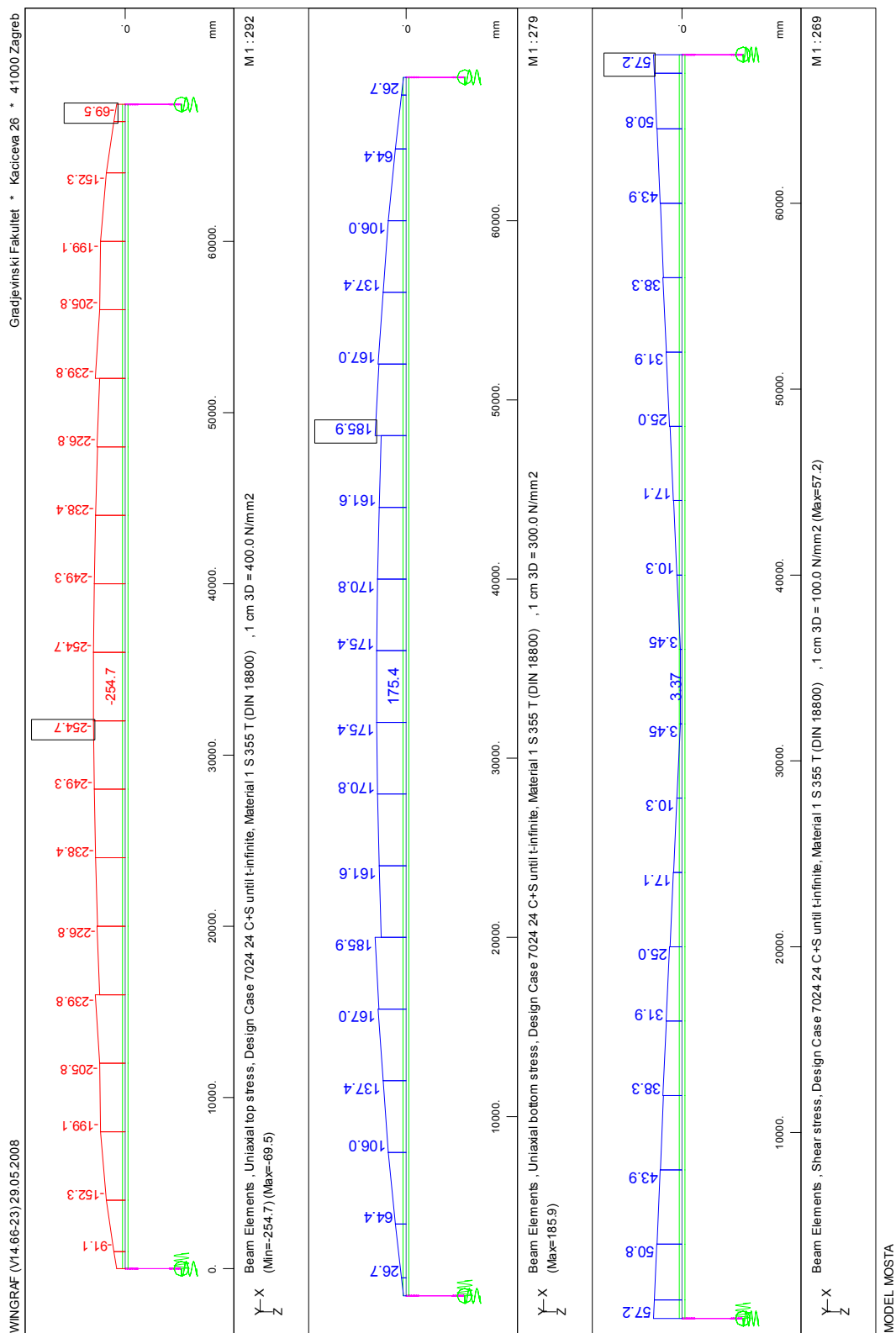
Reakcije: Stalno + dodatno stalno



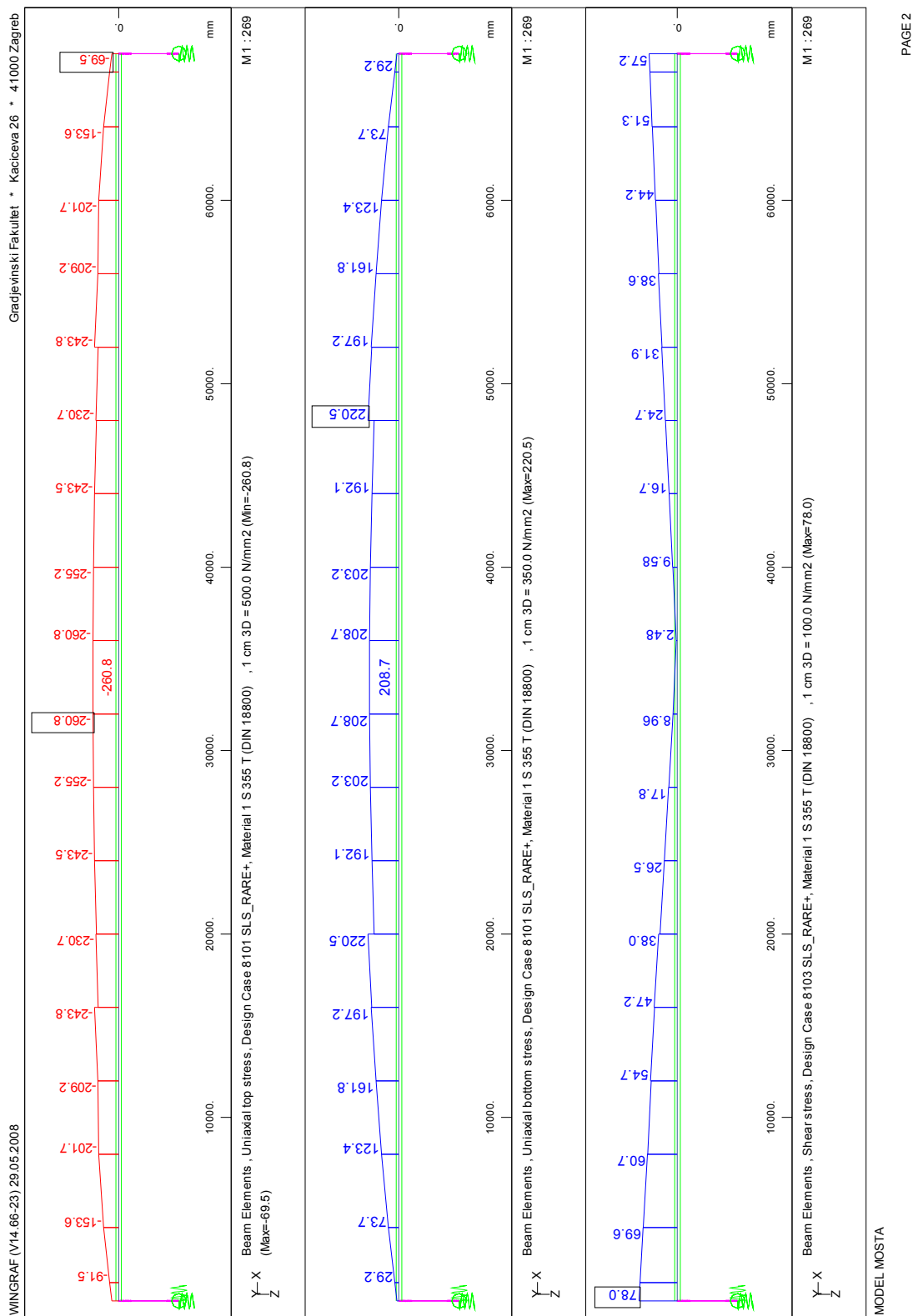


Reakcije: Promet-koncentrirano

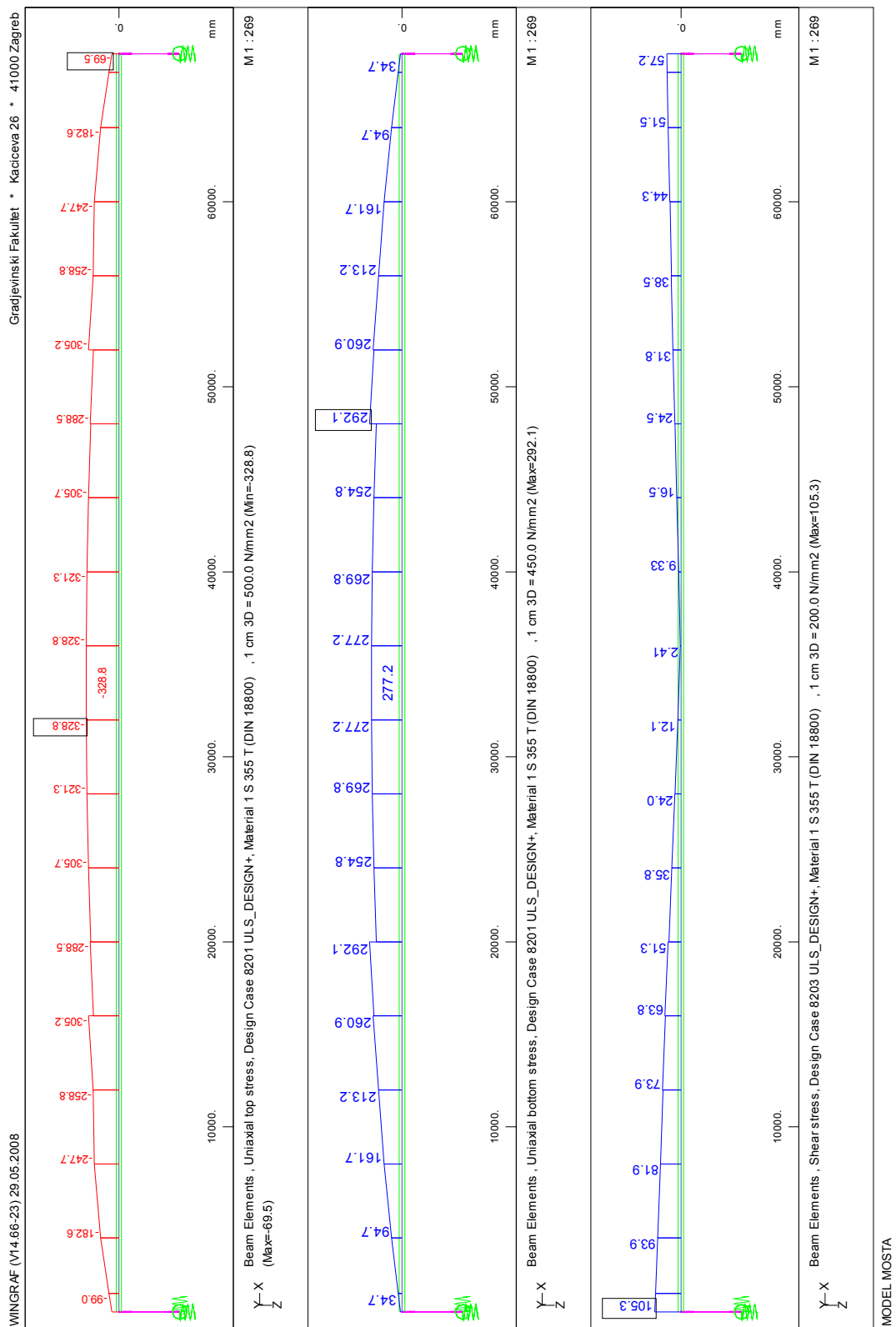




Naprezanja u čeliku: Stalno + dodatno stalno + puzanje i skupljanje

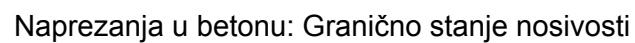


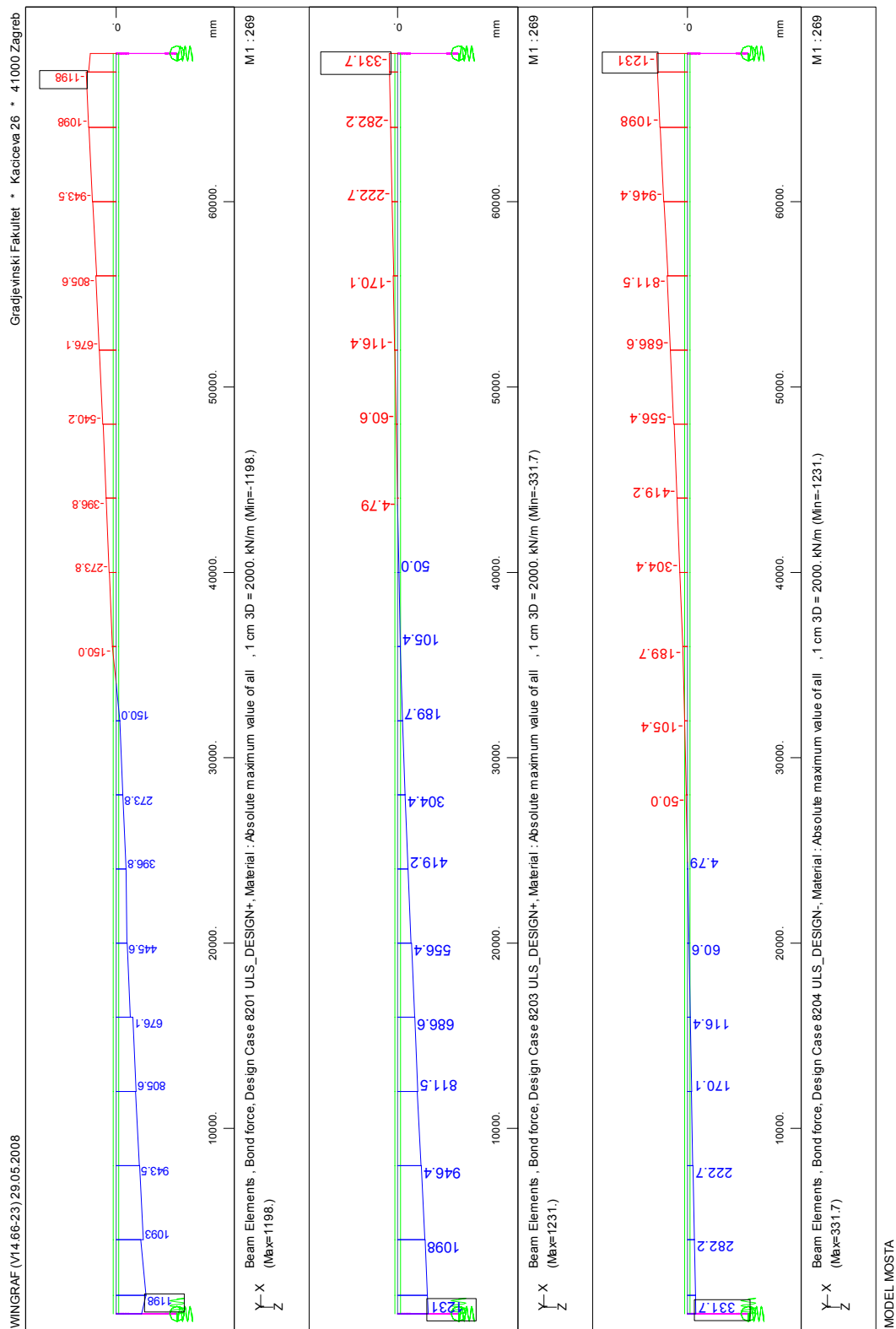
Naprezanja u čeliku: Granično stanje uporabljivosti



PAGE 3

Naprezanja u čeliku: Granično stanje nosivosti





Posmična sila na spoju čelika i betona

VRSTA NAPREZANJA	DEBLJINA LAMELE	GRANIČNA NAPREZANJA
VLAK	$t \leq 40 \text{ mm}$	$\sigma_{\text{dop}} = 355 \text{ MPa}$
	$40 \text{ mm} < t \leq 100 \text{ mm}$	$\sigma_{\text{dop}} = 335 \text{ MPa}$
TLAK	$t \leq 40 \text{ mm}$	$\sigma_{\text{dop}} = 355/1,1 = 322,73 \text{ [Mpa]}$
	$40 \text{ mm} < t \leq 100 \text{ mm}$	$\sigma_{\text{dop}} = 335/1,1 = 304,55 \text{ [Mpa]}$
POSMIK	$t \leq 40 \text{ mm}$	$\tau_{\text{dop}} = \frac{355}{(1,1 \times \sqrt{3})} = 186,33 \text{ [MPa]}$
	$40 \text{ mm} < t \leq 100 \text{ mm}$	$\tau_{\text{dop}} = \frac{335}{(1,1 \times \sqrt{3})} = 175,83 \text{ [MPa]}$

Dokaz nosivosti za GSN

$$\sigma_{\text{Ed,max}} \leq \sigma_{\text{dop}}, \quad \tau_{\text{Ed,max}} \leq \tau_{\text{dop}}$$

		$\sigma_{\text{Ed,max}},$ $\tau_{\text{Ed,max}}$ (MPa)		$\sigma_{\text{dop}},$ τ_{dop} (MPa)	NE ZADOVOLJAVA / ZADOVOLJAVA
POLJE	Tlak	-328,2	>	304.54	NE ZADOVOLJAVA
	Vlak	277.2	<	355	ZADOVOLJAVA
	Posmik	105.3	<	186,33	ZADOVOLJAVA

Ne zadovoljava tlačno naprezanje u gornjem pojasu, pa je potrebno povećati dimenzije (širinu i debljinu).

Dokaz nosivosti za GSU

$$\sigma_{Ed,max} \leq \sigma_{dop}, \quad \tau_{Ed,max} \leq \tau_{dop}$$

		$\sigma_{Ed,max}$, $\tau_{Ed,max}$ (MPa)		σ_{dop} , τ_{dop} (MPa)	NE ZADOVOLJAVA / ZADOVOLJAVA
POLJE	Tlak	-2608	>	304.54	ZADOVOLJAVA
	Vlak	208.7	<	355	ZADOVOLJAVA
	Posmik	78.0	<	186,33	ZADOVOLJAVA

Reinforcement after min-bew + crack design

mm

60000.

50000.

40000.

30000.

20000.

10000.

0

65390

65390

65390

1.0271E5

1.0188E5

1.6599E5

1.0979E5

1.0979E5

65390

65390

1.0979E5

1.0979E5

1.6599E5

1.0188E5

1.0271E5

65390

65390

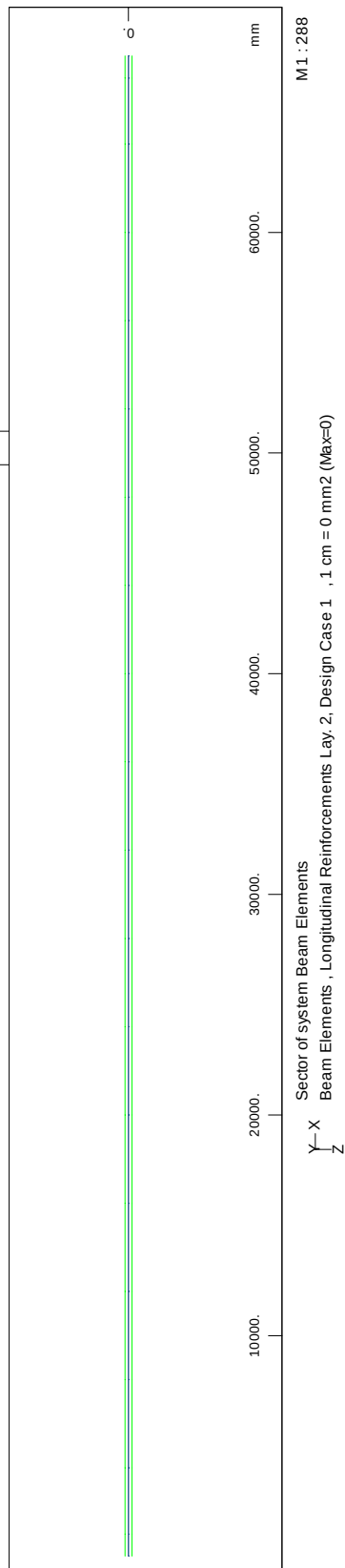
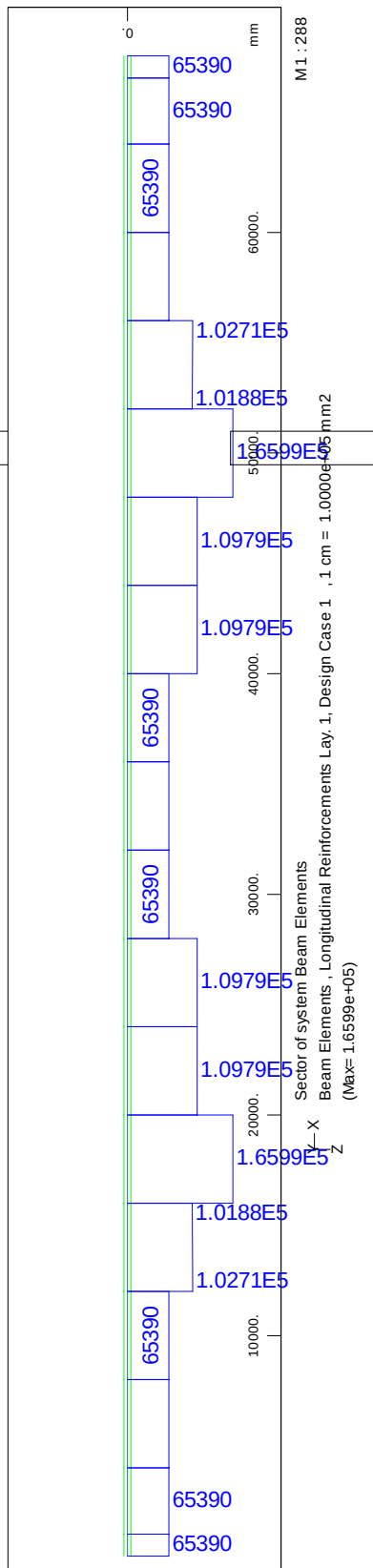
M 1 : 288

Sector of system Beam Elements

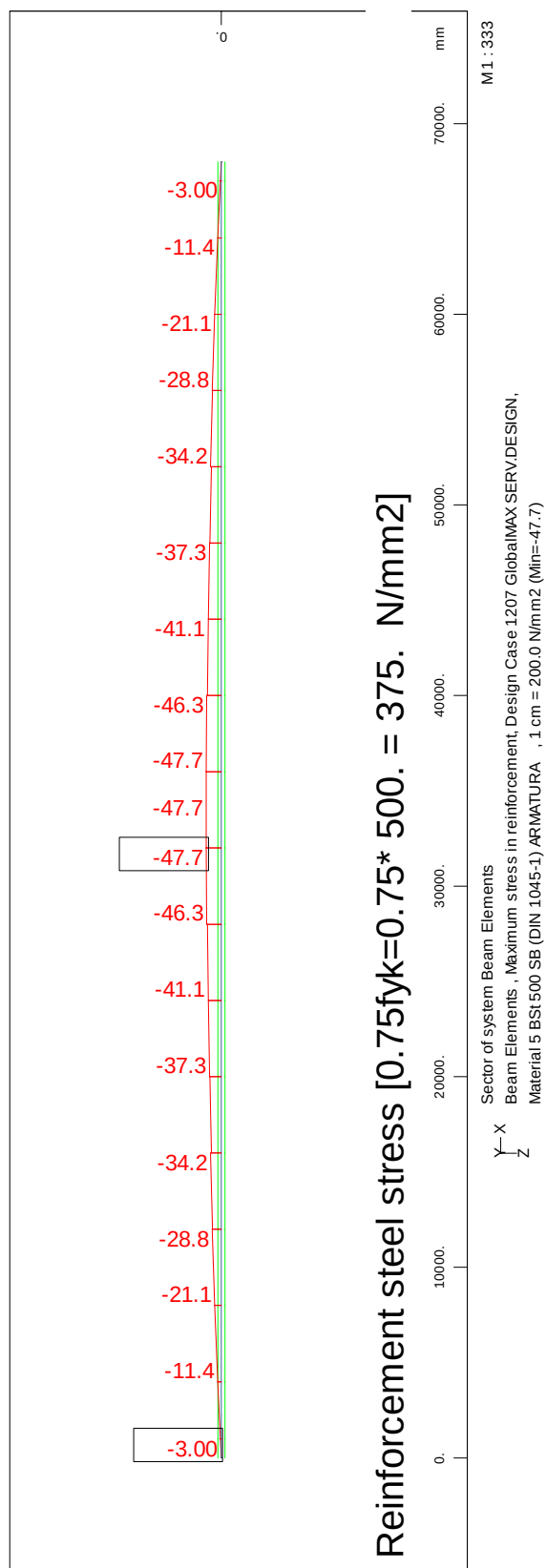
Beam Elements , Longitudinal reinforcements (total), Design Case 1 , 1 cm = 1.0000e+05 mm2

(Max= 1.6599e+05)

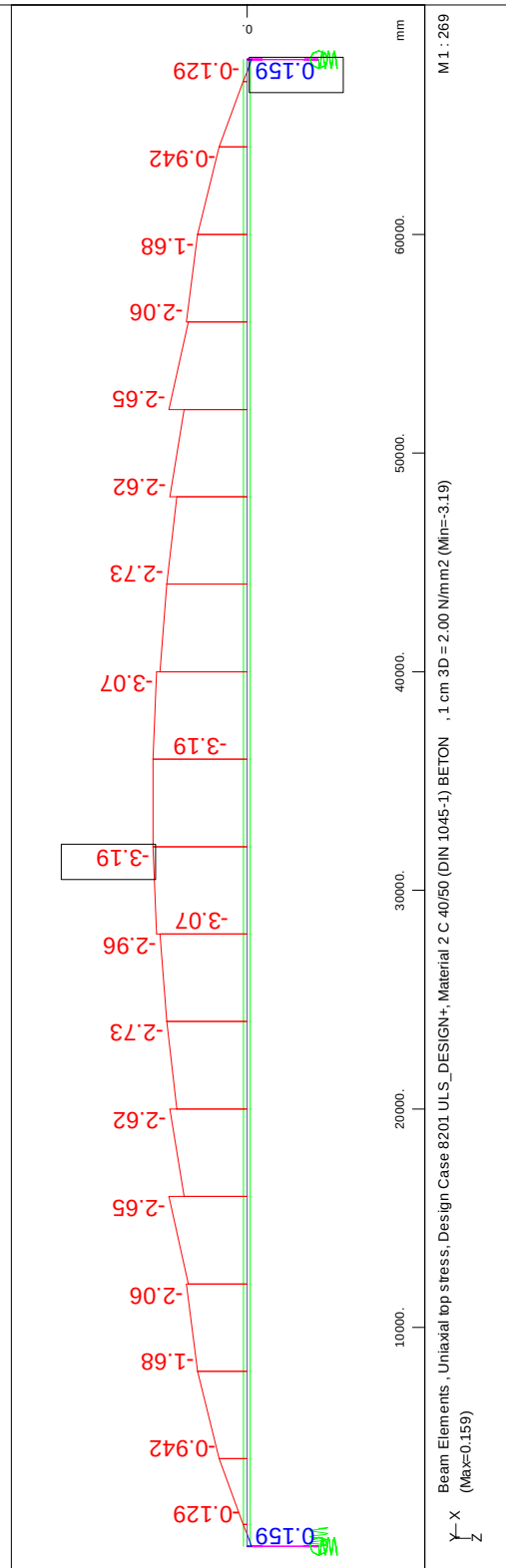
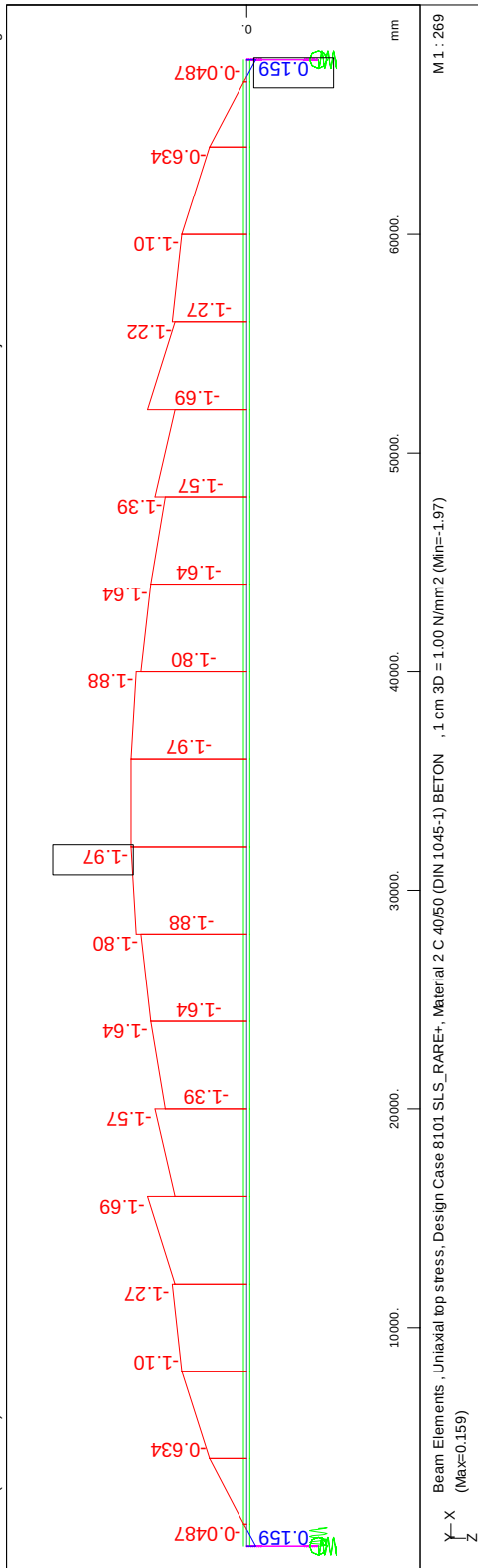
Y X Z



Potrebna površina armature



Naprezanja u armaturi



Naprezanja u betonu za GSU i GSN

